


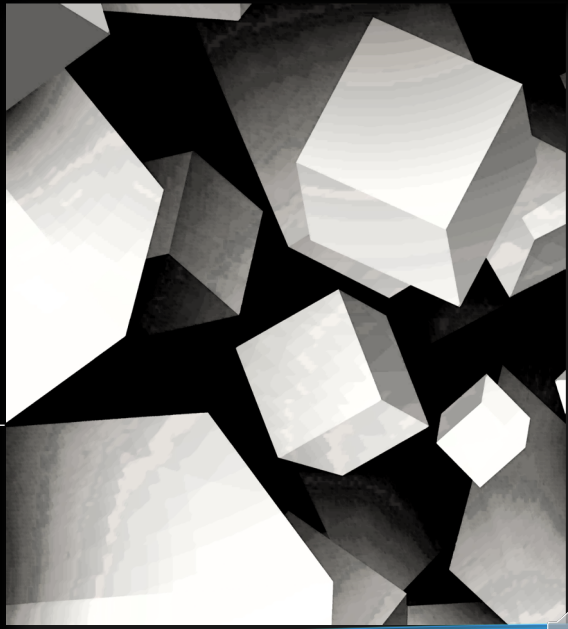
2021 FALL TOPICAL CONFERENCE  
UNCONVENTIONAL PETROPHYSICS



Upscaling borehole resistivities to 3D  
anisotropic models for CCUS applications

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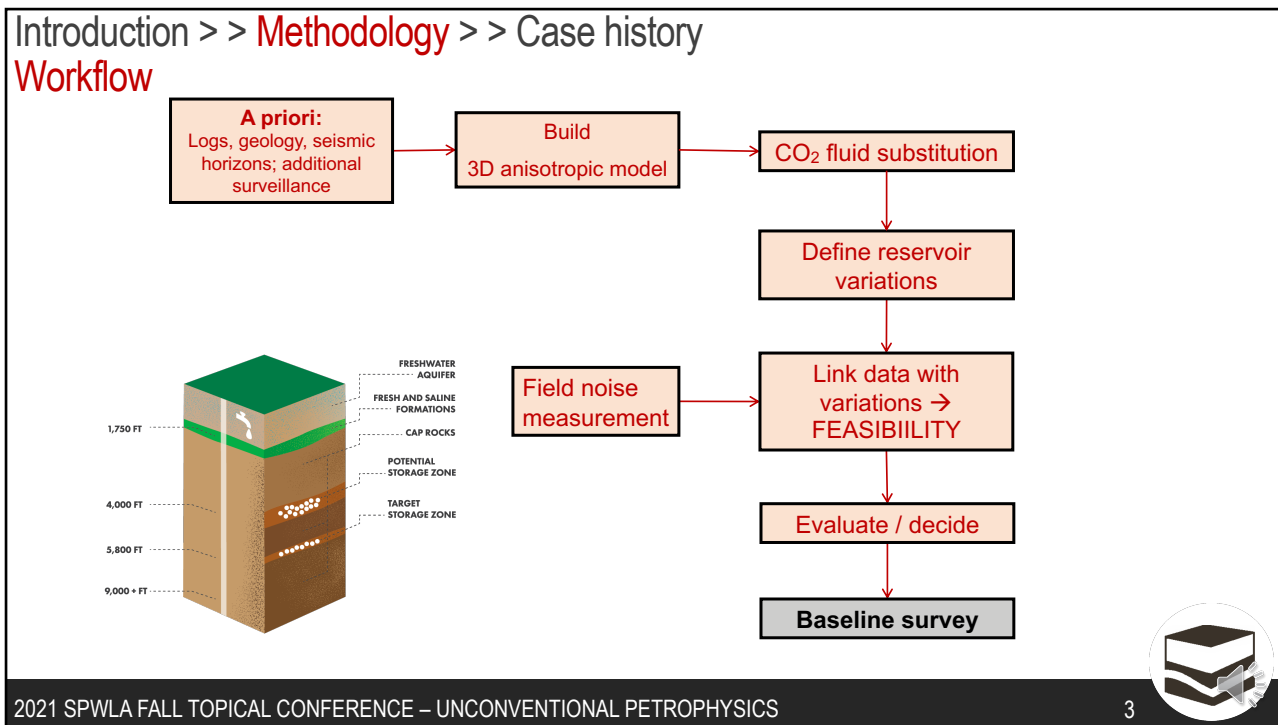
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Introduction

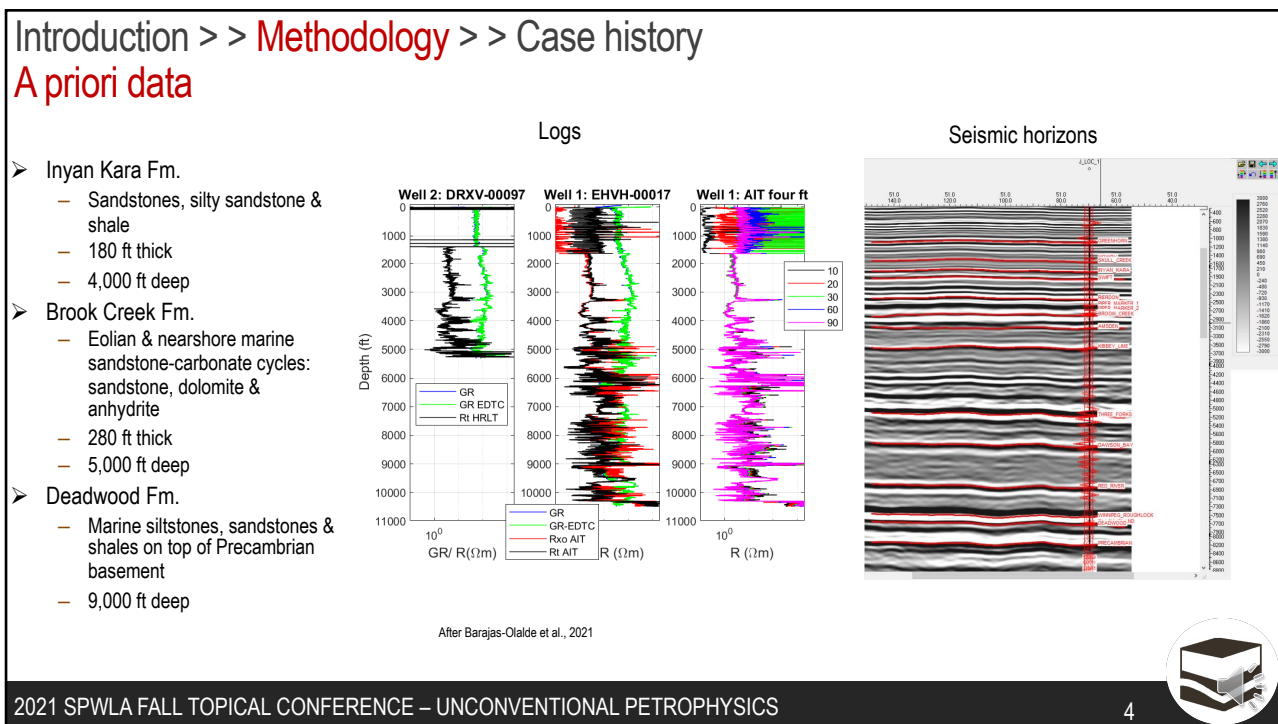
- Monitor CO<sub>2</sub> reservoir fluid movement
- Fluid sensitivity asses with 3D models
- Workflow to upscale from borehole to surface
- Derived CO<sub>2</sub> resistivity from petrophysics
- Field examples, validation



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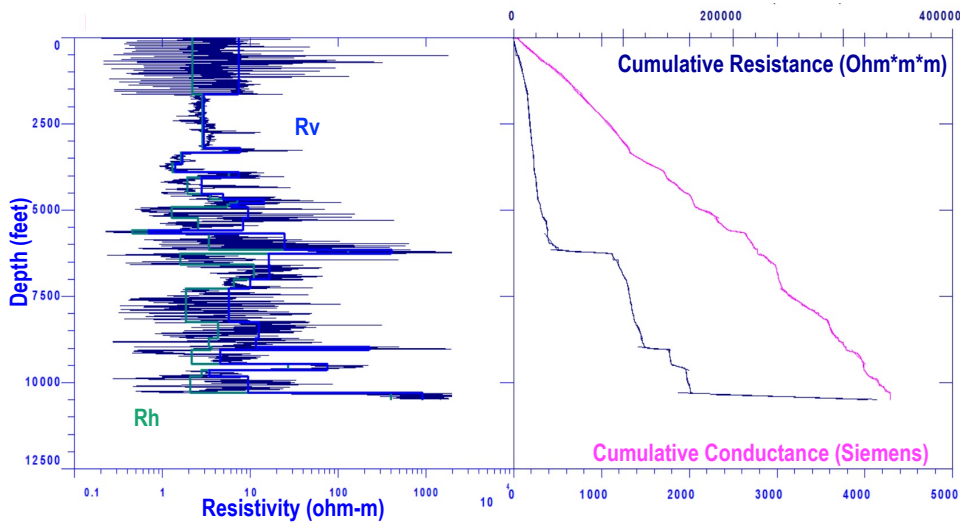


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**Anisotropic model**

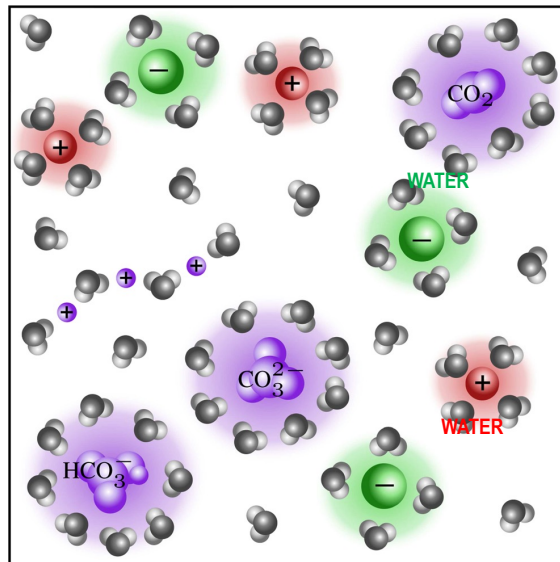


- 31 layers
- Use
  - Rv for CSEM – E field
  - Rh for CSEM – H field
  - Rh for MT



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**Dissolved CO<sub>2</sub> – how does it influence rock resistivity?**

- @ normal brine salinity → fluids are more resistive (6 -50 times)
- @ low salinity (≤ 5,000 ppm) → more conductive



After Boerner et al., 2015



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### CO<sub>2</sub> fluid substitution

#### Know petrophysical parameters:

Inyan Kara Fm.: Average porosity: 20 %, average permeability: 200 mD

Broom Creek Fm.: Average porosity sandstone: 23 %, average permeability sandstone: 222 mD

Deadwood Fm.: Average porosity sandstone: 11 %, average permeability sandstone: 70 mD

#### Assumptions:

Brine salinity: 20,000 ppm for all reservoirs

CO<sub>2</sub> density: ~ 1000 kg/m<sup>3</sup>

Geothermal gradient 1.82 °C/100 m



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### CO<sub>2</sub> fluid substitution - continued

Estimate formation temperature for each reservoir

$R_w$  calculated from Schlumberger chart of temperature & NaCl concentration

Using the formula:

$$F = \frac{a}{\phi^m}$$

Where  $a = 1$  &  $m = 2$

Then using

$$R_0 = F \times R_w$$

we determine the formation resistivity for the sandstone.

If shaly sand, the one can use

$$\frac{1}{R_t} = \frac{1 - V_{sh}}{R_0} + \frac{V_{sh}}{R_{sh}}$$

Formation resistivity was compared to average resistivity (Rh) from well data, values were consistent, validate selected  $a$  &  $m$  constants



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### CO<sub>2</sub> formation resistivity

Given CO<sub>2</sub> is 10 times more resistive than brine →

$$R_{CO_2} = F \times (10 \times R_w)$$

Average resistivity for brine volume and CO<sub>2</sub> volume, we calculate the resistivity change ratio for 100 % water saturation → vertical resistivity

Reference: resistivity 6 to 50 times higher than fresh water (\*10 for brine) (Capobianco et al, final version 071814, contract No. DE-AC05-00OR22725)



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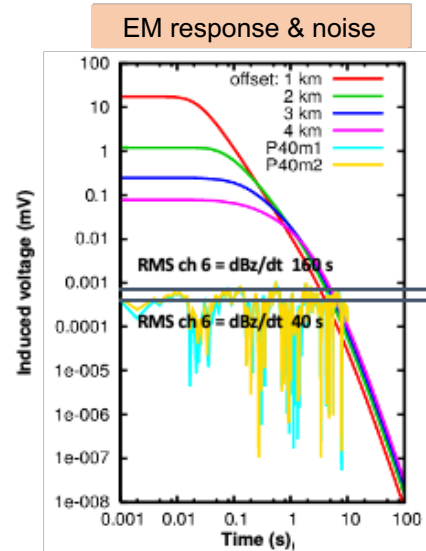
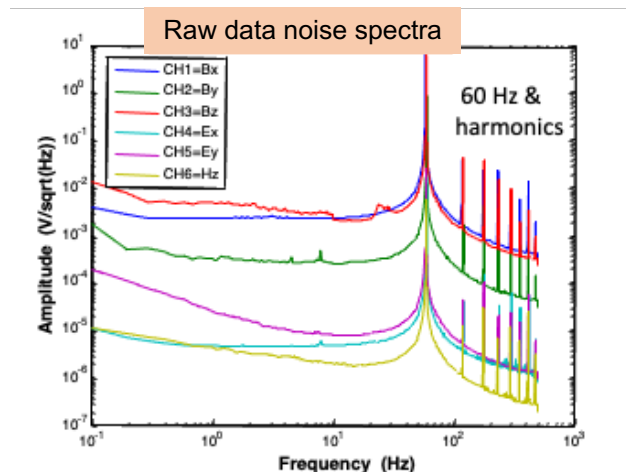
### 3D modeling scenarios

| Reservoir                 | Years of injection | Radius of injection area (m) | Ratio of increase of resistivity by saturation of CO <sub>2</sub> |      |      | Resistivity by saturation of CO <sub>2</sub><br>R <sub>h</sub> & R <sub>v</sub> (Ωm) |                        |                        | Brine saturated resistivity (Ωm)                |
|---------------------------|--------------------|------------------------------|---|------|------|--|------------------------|------------------------|---|
|                           |                    |                              | 90 %  | 60 % | 30 % | 90 %   | 60 %                   | 30 %                   |   |
| Broom Creek<br>(5,000 ft) | 1                  | 200                          | 16.4  | 4.2  | 2.7  | R <sub>h</sub> : 22.46   | R <sub>h</sub> : 5.75  | R <sub>h</sub> : 3.69  | R <sub>h</sub> : 1.37<br>R <sub>v</sub> : 15.35 |
|                           | 5                  | 500                          |   |      |      | R <sub>v</sub> : 251.74  | R <sub>v</sub> : 64.47 | R <sub>v</sub> : 41.44 |   |
|                           | 15                 | 860                          |   |      |      |  |                        |                        |   |
| Deadwood<br>(9,000 ft)    | 1                  | 150                          | 7.5   | 2.3  | 1.5  | R <sub>h</sub> : 17.62   | R <sub>h</sub> : 5.4   | R <sub>h</sub> : 3.52  | R <sub>h</sub> : 2.35<br>R <sub>v</sub> : 24.9  |
|                           | 5                  | 230                          |   |      |      | R <sub>v</sub> : 186.75  | R <sub>v</sub> : 57.27 | R <sub>v</sub> : 37.35 |   |
|                           | 15                 | 610                          |   |      |      |  |                        |                        |   |
| Inyan* Kara<br>(4,000 ft) | 1                  | 300                          | 10  | 2.6  | 1.5  | R <sub>h</sub> : 57  | R <sub>h</sub> : 14.82 | R <sub>h</sub> : 8.55  | R <sub>h</sub> : 5.7<br>R <sub>v</sub> : 7.29   |
|                           | 5                  | 660                          |   |      |      | R <sub>v</sub> : 72.9  | R <sub>v</sub> : 18.95 | R <sub>v</sub> : 10.93 |   |
|                           | 15                 | 1150                         |   |      |      |  |                        |                        |   |

Volume of injection of 3 million tons for reservoir Brook Creek and 0.5 million for Deadwood  
Inyan Kara Fm. is just backup for injection



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Field noise measurements

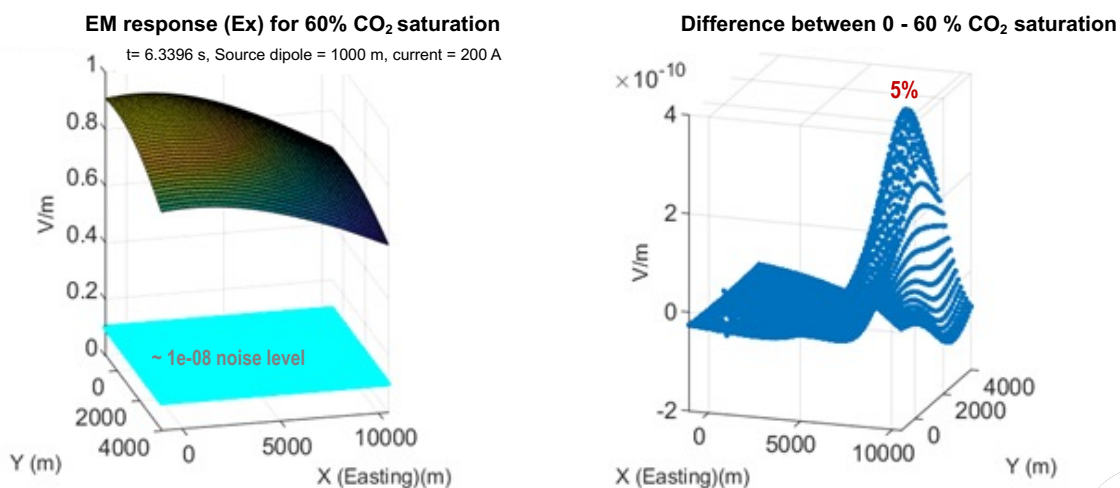


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EM sensitivity & field data results

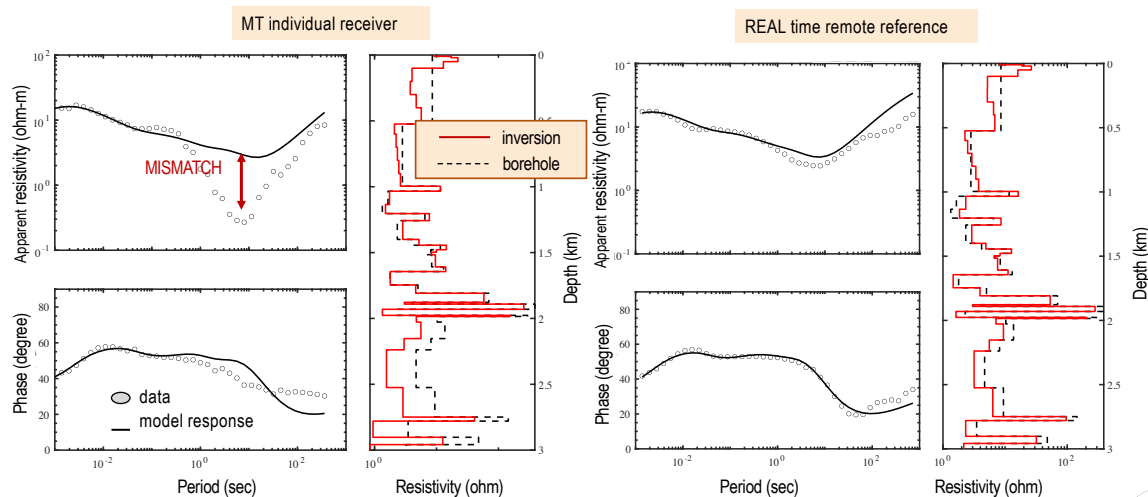
- EM sensitivity
  - Broom Creek Fm. (5,000 ft deep) – detectable in 5% range
  - Deadwood Fm. (9,000 ft deep) – around 1%
  - Inyan Kara Fm. (4,000 ft deep) - > than 5 %
- CSEM signal > noise level to 4-6 s.
- 1D & 2D MT inversion
- CSEM inversion



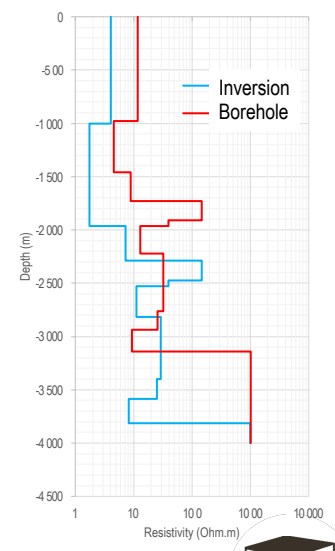
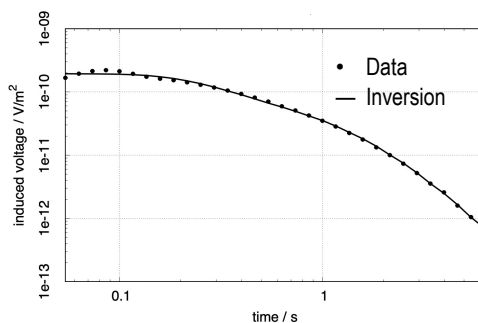
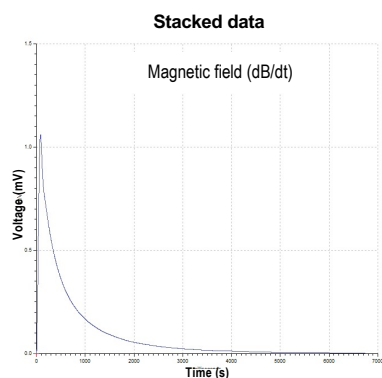
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 Example modeled CSEM response



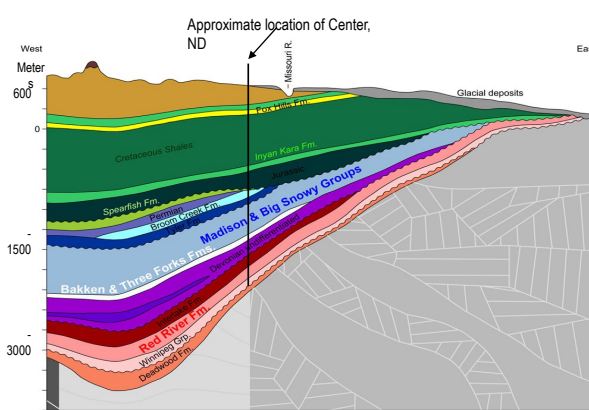
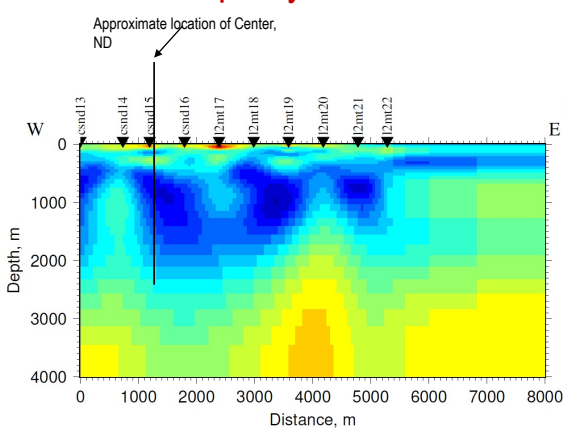
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 Cloud-based quality assurance: MT



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 Cloud-based quality assurance: CSEM



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 Cloud-based quality assurance: 2D MT



After Barajas-Olalde et al., 2021

After Barajas-Olalde et al., 2021





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Conclusions

- EM monitors fluid movements
- CO<sub>2</sub> flooding provides resistivity contrast → EM anomaly
- CSEM preferred method
- MT & CSEM QA inversion results match anisotropic log model
- Upscaling workflow validated
- Future: CO<sub>2</sub> injection & time-lapse measurements

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Thank you!

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